

## FOLLETT CORPORATION

### 25/50 CI425 A/W DISPENSERS

DES. **J. ROBERSON**

JOB NO. **11-1420**

DATE **6/10/14**

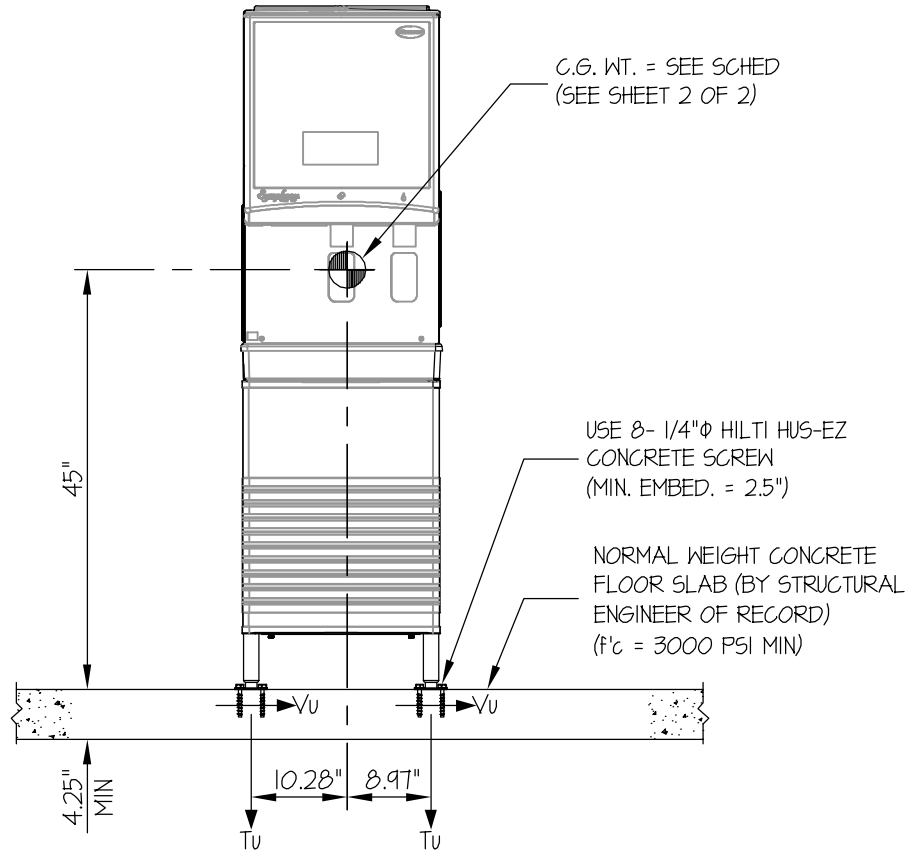
SHEET

**1**

OF **2** SHEETS

SEISMIC ANCHORAGE

SLAB ON GRADE



**FRONT ELEVATION**

**NOTES:**

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10 STRENGTH DESIGN IS USED. ( $S_Ds = 2.30$ ,  $a_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $\Omega_0 = 2.5$ ,  $z/h = 0$ )

HORIZONTAL FORCE ( $E_h$ ) =  $1.035 W_p$

HORIZONTAL FORCE ( $E_{mh}$ ) =  $2.59 W_p$  (FOR CONCRETE ANCHORAGE)

VERTICAL FORCE ( $E_v$ ) =  $0.46 W_p$

- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.

*Jonathan Roberson*  
 REGISTERED PROFESSIONAL ENGINEER  
 No. 4197  
 EXP. 6-30-2016  
 6/10/14  
 STATE OF CALIFORNIA

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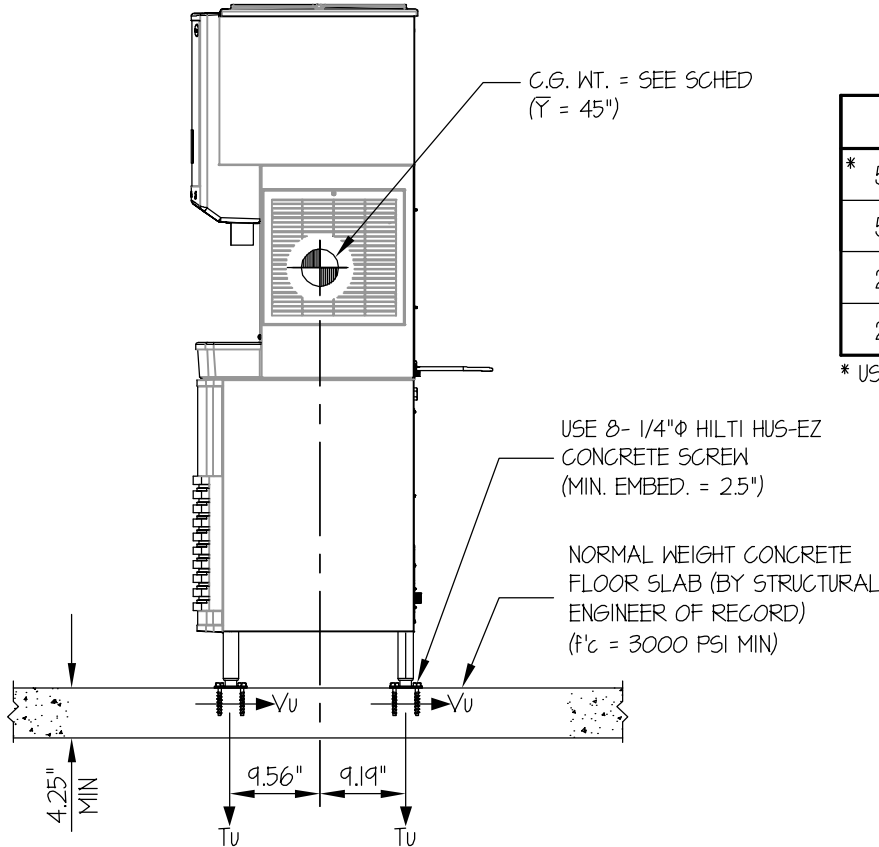
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MODEL	MAX WT	T <sub>u</sub>	V <sub>u</sub>
* 50CI425W	276	569	95
50CI425A	271	559	94
25CI425W	249	514	86
25CI425A	244	503	84

\* USED IN CALCULATION

### SIDE ELEVATION

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

(STRENGTH DESIGN IS USED) ( $S_Ds = 2.30$ ,  $a_p = 10$ ,  $I_p = 15$ ,  $R_p = 2.5$ ,  $\Omega_o = 2.5$ ,  $z/h = 0$ )

WEIGHT = 276 LB

HORIZONTAL FORCE ( $E_{mh}$ ) =  $2.59 W_p = 715$  LB

VERTICAL FORCE ( $E_v$ ) =  $0.46 W_p = 127$  LB

BOLT FORCES:

BOLT SPEC: 1/4" HILTI HUS -EZ

$\phi T = 0.75 \phi N_n = 623$  LB/BOLT (TENSION)

$\phi V = \phi V_n = 836$  LB/BOLT (SHEAR)

TENSION (T)

$$T_u \text{ MAXIMUM} = \left[ \frac{715\#(45\")(9.56\"){}}{2 \text{ BOLTS}(19.25\")(18.75\")} \times (0.3) \right] + \frac{715\#(45\")(10.28\"){}}{2 \text{ BOLTS}(18.75\")(19.25\")} - \frac{(276\#(0.9) - 127\#)(10.28\")(9.56\"){}}{2 \text{ BOLTS}(19.25\")(18.75\")} = 569 \text{ LB/BOLT (MAX)}$$

( HORIZ - FRONT TO BACK )                      ( HORIZ - SIDE TO SIDE )                      ( 0.9WEIGHT) - E<sub>v</sub>)

SHEAR (V)

$$V_u \text{ MAXIMUM} = \frac{715\#(10.28\"){}}{4 \text{ BOLTS}(19.25\")} = 95 \text{ LB/BOLT (MAX)}$$

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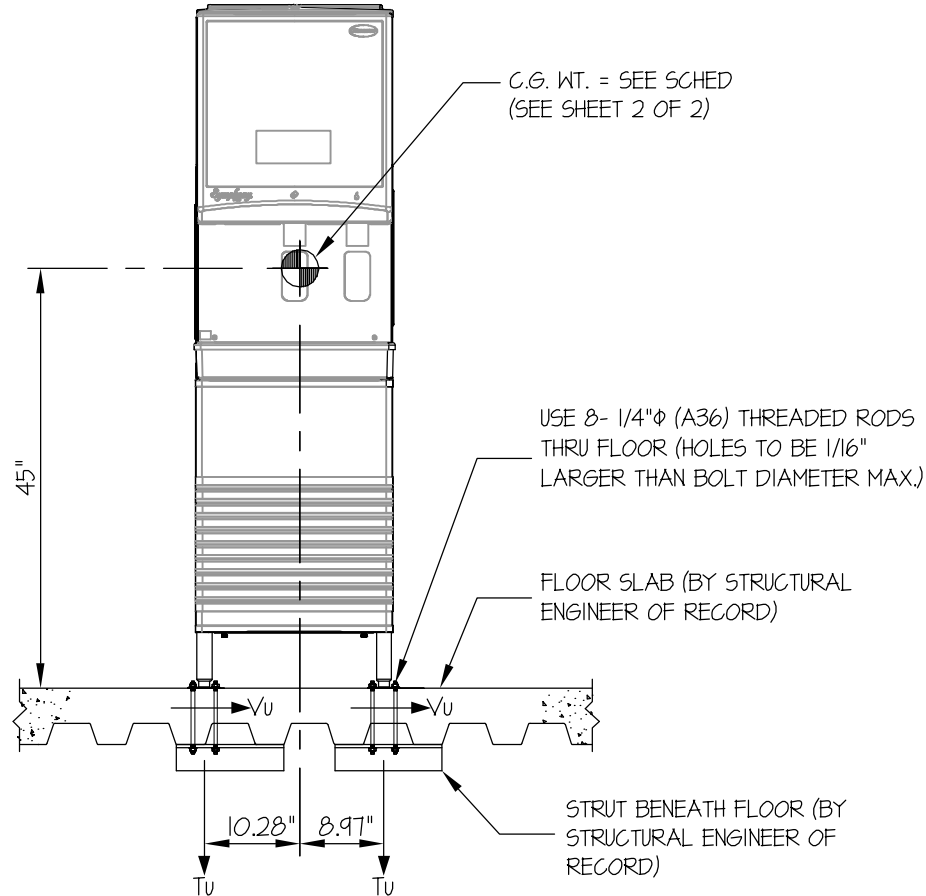
SHEET

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SEISMIC ANCHORAGE

UPPER FLOOR



**FRONT ELEVATION**

NOTES:

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10 STRENGTH DESIGN IS USED. ( $S_{ds} = 2.50$ ,  $\alpha_p = 1.0$ ,  $I_p = 1.5$ ,  $R_p = 2.5$ ,  $\Omega_0 = 2.5$ ,  $z/h \leq 1$ )

HORIZONTAL FORCE ( $E_h$ ) =  $1.80 W_p$

VERTICAL FORCE ( $E_v$ ) =  $0.50 W_p$

- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THESE CALCULATIONS ENCOMPASS ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
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JONATHAN ROBERSON  
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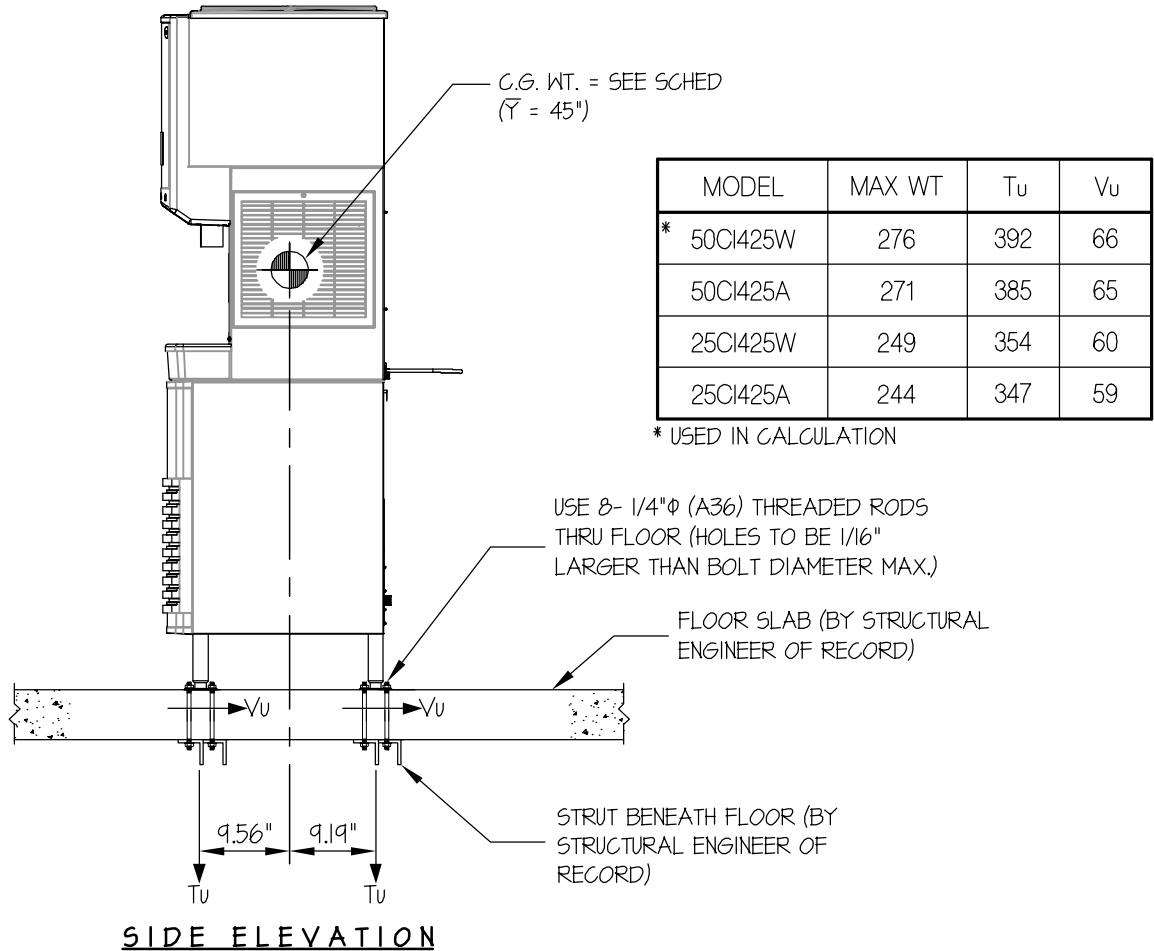
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SEISMIC ANCHORAGE

UPPER FLOOR



LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

(STRENGTH DESIGN IS USED) ( $S_{ds} = 2.5$ ,  $a_p = 1.0$ ,  $I_p = 2.5$ ,  $R_p = 2.5$ ,  $z/h \leq 1$ )

WEIGHT = 276 LB

HORIZONTAL FORCE ( $E_h$ ) = 180  $W_p$  = 497 LB

VERTICAL FORCE ( $E_v$ ) = 0.50  $W_p$  = 138 LB

BOLT FORCES:

BOLT SPEC: 1/4" phi (A36) THREADED ROD

$\phi T$  = 1599 LB/BOLT

$\phi V$  = 853 LB/BOLT

TENSION (T)

$$T_{u \text{ MAXIMUM}} = \left[ \frac{497\#(45\")(9.56\"){}}{2 \text{ BOLTS}(19.25\")(18.75\")} \times (0.3) \right] + \frac{497\#(45\")(10.28\"){}}{2 \text{ BOLTS}(18.75\")(19.25\")} - \frac{(276\#(0.9) - 138\#)(10.28\")(9.56\"){}}{2 \text{ BOLTS}(19.25\")(18.75\")} = 392 \text{ LB/BOLT (MAX)}$$

( HORIZ - FRONT TO BACK )                      ( HORIZ - SIDE TO SIDE )                      ( 0.9(WEIGHT) - E<sub>v</sub> )

SHEAR (V)

$$V_{u \text{ MAXIMUM}} = \frac{497\#(10.28\"){}}{4 \text{ BOLTS}(19.25\")} = 66 \text{ LB/BOLT (MAX)}$$